WORKSHOP

Mode II interlaminar fracture toughness and the factors affecting it

CERTBOND Project: Mode-II quasi static characterization of co-cured composite adhesive joints

Serafín Sánchez-Carmona, Alberto Barroso





May 13th, 2025

Mode-II quasi static characterization of co-cured composite adhesive joints









Mode I: Static and Fatigue



Mode II: Static and Fatigue

Failure prediction (static & fatigue) of co-cured single-lap joints.





Mode-II quasi static characterization of co-cured composite adhesive joints







Round Robin Exercise

Participants



EPFL

Univ. Minho

Univ. Seville

Univ. Girona

Univ. Patras

Univ. Aveiro

Univ. Bayreuth

Univ. Nantes

Polit. Milano

Univ. East Sarajevo

TU Delft



Delft University of Technology





QS

Х

X

Х

X

X

UNIVERSITY OF PATRAS

Fat

Х

Х

Х

Х

X

X

Х



УНИВЕРЗИТЕТ У ИСТОЧНОМ САРАЈЕВУ University of East Sarajevo

SLJ

Fat

Х



Х

X

Х

universidade de aveiro









Mode-II quasi static characterization of co-cured composite adhesive joints

INTERNATIONAL STANDARD

ISO 15114

First edition 2014-05-15



Designation: D7905/D7905M – 19^{ε1}

Standard Test Method for Determination of the Mode II Interlaminar Fracture Toughness of Unidirectional Fiber-Reinforced Polymer Matrix Composites¹

This standard is issued under the fixed designation D7905/D7905M; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

ε1 NOTE-Editorial changes were made to Table 1 in November 2019.

Fibre-reinforced plastic composites — Determination of the mode II fracture resistance for unidirectionally reinforced materials using the calibrated end-loaded split (C-ELS) test and an effective crack length approach





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ISO 15114:2014(E)

Introduction

Previous attempts to determine mode II delamination resistance curves (R-curves) for composites have been hampered by the experimental difficulty of determining crack length in the absence of any applied beam opening displacement and when a complex damage zone develops ahead of the crack front. The effects of friction in the different mode II test specimens have also been widely debated and have typically been determined to introduce errors of between 1 % and 3 % in $G_{\rm IIC}$ determination for ELS specimens (n.b. friction effects would appear to be more significant in 3 point loaded end notch flexure (3ENF) (to be standardized by ASTM) and, particularly, in the 4 point loaded (4ENF) test specimen. Stabilized ENF was not popular in round-robin trials).

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Manufacturing of samples









I-2.4	П-2.К П-2.15	
1-2.5	I-2.14	
I-2.5 I-2.7	Ц-2.13 11-2 12	
E-2.8	II-2.1	
E-2.9	II-2.10	



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1. Lab_3. Four specimens with an unexpected much higher failure load \Rightarrow discarded

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- 1. Lab_3. Four specimens with an unexpected much higher failure load \Rightarrow discarded
- 2. Criterion for unloading (crack advance vs load drop) (see one specimen in Lab_2)
- 3. Test duration. One simple loading&unloading ≈ 6 minutes. Each sample 6 L&U ⇒ 36 min. A set of 6 samples may take 4 or 5 hours !!!

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	Lab_1		Lab_2	
	NPC	PC	NPC	PC
G _{IIC} (kJ/m2)	3.15	2.66	2.69	2.21
desvest (kJ/m2)	0.57	0.22	0.26	0.39
CoV (%)	18.0	8.2	9.5	17.8

1. Fracture Toughness is lower for the PC specimen.

- No clear trend for scatter in results
 For Lab_1 much higher in the NPC tests.
 For Lab_2 much higher in the PC tests.
- 3. Doubts regarding the requirement of recording the unloading stage.

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